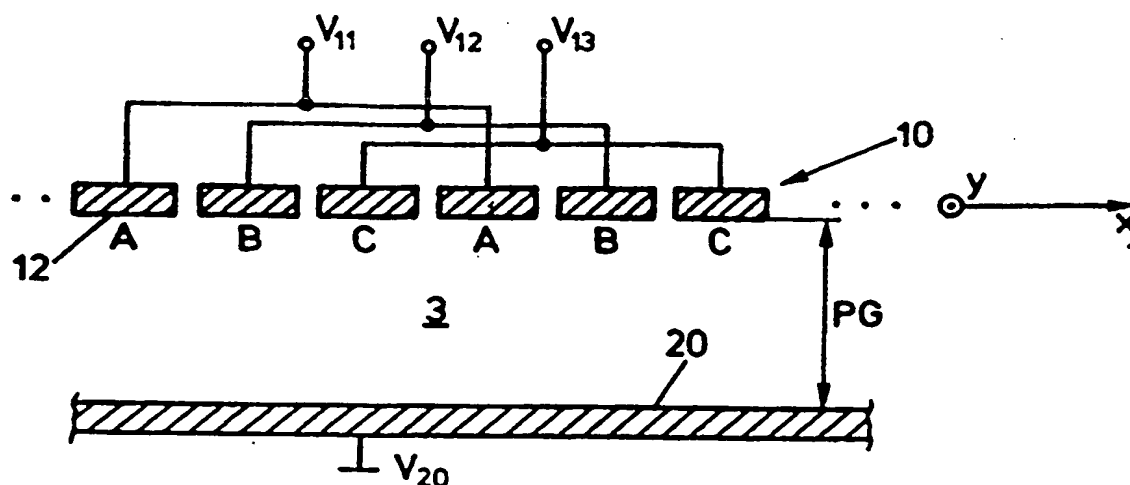




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(54) Title: CAPACITIVELY COUPLED RF-PLASMA REACTOR



(57) Abstract

In a capacitively coupled RF-plasma reactor, whereat a discharge area (3) is provided between a pair of distant electrodes (10, 20), at least one of these electrodes (10) is subdivided into a multitude of sub-electrodes (12), which are operated in groups (A, B, C) on respective electrical signals. By appropriately selecting amplitude, phasing, spectral content of these signals (V_{11} to V_{13}), a desired distribution of treatment effect on a workpiece deposited on the second electrode (20) may be realised, especially for treating large-area workpieces.

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Capacitively coupled RF-plasma reactor

Background of the invention

Customary, capacitively coupled RF-plasma reactors comprise first and second mutually spaced electrodes which concomitantly confine the plasma reaction volume. Besides of the two electrodes, their electrode conductive surfaces, no further electroconductive parts act as a third electrode with an externally applied electrical potential into the plasma reaction volume. Therefore, typical capacitively coupled RF-plasma reactors are also said "diode type" reactors. Confining the plasma reaction volume between the two electrodes which are mutually driven at electric RF potential is normally achieved in providing a spacing at the border of the two electrodes which suffices for electric isolation in terms of DC, but which prevents spreading of the plasma discharge outside the space confined by the two electrodes. This may be achieved e.g. by spacing the two electrodes at their periphery by a distance smaller than dark space distance at the respective operating conditions.

Such capacitively coupled RF-plasma reactors have been used for many years in the field of plasma processing, especially for treating flat substrates such as silicon wafers.

The most common applications of such reactors are Plasma-Enhanced Chemical Vapour Deposition (PECVD) and Plasma Dry Etching. Plasma Dry Etching can be divided into Reactive Ion Etching (RIE), in which ion bombardment is used to promote an anisotropic etching, or in Plasma Etching (PE), in which ion bombardment is to be avoided.

Plasma cleaning, removal of a polymer resist (Ashing) or plasma induced surface activation of workpieces can also be

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performed in a capacitively coupled RF plasma reactor. Most such reactors are construed with planar electrodes.

In these applications the plasma is generated by a driving RF voltage, most commonly for industrial applications at a frequency of 13.56 MHz.

An RF-driven plasma develops a large self bias voltage between the plasma and the plasma reaction volume surrounding walls which are, as was stated, the electrode surfaces. This is due to the rectifying effect of the RF voltage across the plasma sheath by the plasma sheath according to the dark space adjacent to each of the electrode surfaces towards the plasma discharge or reaction volume. As a consequence, in a classical capacitively coupled RF reactor the ion bombardment of the workpiece or substrate is governed by the ratio between the two electrode surface areas which are in contact with the plasma discharge. Most plasma self bias, enhancing ion bombardment, arises adjacent to the electrode surface of the smaller electrode area, and the potential difference across the sheath or dark-space adjacent to the larger area electrode is accordingly smaller. This effect is conveniently exploited by plasma process designers to tailor the ion bombardment on the substrate. E.g. for RIE the workpiece or substrate is placed adjacent or on the smaller-area electrode coupled to the plasma which results in larger ion bombardment. Inversively, for PE the workpiece is placed adjacent or on the larger-area electrode where ion bombardment is smaller.

There is today a need for plasma processing of large surface workpieces as e.g. of large surface glass plates. E.g. the flat display industry is today considering manufacturing on such plates of about 1 m². The type of processes to be performed to produce the pixel related electronic circuits on

such glass plates are of the same nature as the processes used in micro-electronics, but have to be performed on significantly larger surface workpieces.

If a large surface substrate is to be processed by a capacitively coupled RF plasma reactor and at process conditions similar to those as used when treating silicon wafers, the plasma gap (the distance between the two electrodes, e.g. of a planar capacitive reactor) must be kept at the predetermined value in order to achieve the number of collisions for excited species as desired. Thus, a typical value for plasma gap is between 1 and 10 cm (both limits included).

With the large surface workpieces and such plasma gaps the electrodes of the reactor take a very extended aspect ratio and the electrode surface area ratio becomes close to 1. This implies that in a capacitively coupled RF plasma reactor for large surface workpieces there is almost no control of ion bombardment. The ion bombardment occurs substantially equally at both electrode surfaces. Such a situation is strongly limiting processing large-size workpieces and especially large-size substrates by known capacitively coupled RF plasma processes as they were developed for the micro-electronic industry.

Summary of the invention

It is an object of the present invention to provide a capacitively coupled RF plasma reactor which allows treatment of large workpiece surfaces with an accurate control of ion bombardment onto the respective electrode surfaces and thus an adjacent workpiece, be it to a desired low or to a desired high level.

This is inventively achieved by the capacitively coupled RF-

plasma reactor, comprising

- a first and a second electrode arrangement mutually spaced and confining a plasma reaction volume,
- at least one of the electrode arrangements comprising electrically mutually isolated sub-electrodes,
- a first group of the sub-electrodes being commonly connected to a first electric input,
- a second group of the sub-electrodes being commonly connected to a second electric input.

This concept of the novel capacitively coupled RF-plasma reactor thus substitutes at least one of the two customary used reactor electrodes by an array of sub-electrodes which by means of their respective first and second electric inputs may be independently and thus differently electrically operated, usually but not exclusively with RF voltages.

In a most preferred embodiment the sub-electrodes of one group and the sub-electrodes of the second group alternate periodically, thus e.g. one after the other as considered at least along one direction along the subdivided electrode arrangement. In the preferred mode of realisation where sub-electrodes of the at least two sub-electrode groups respectively connected to different electric inputs, especially RF inputs, are periodically alternating, the distance from one sub-electrode connected to one RF input to the next such sub-electrode connected to the same RF input and thus local periodicity of the sub-electrode pattern with respect to their electric feed should be of the order or less than the extent of the plasma gap between the two mutually facing electrode arrangements. This makes sure that the workpiece surface to

be treated is subjected to an "averaged" effect of plasma discharge.

In a simplified consideration it may be said that with the inventive reactor the workpiece surface to be treated is exposed to a multitude of different sub-RF plasma discharges generated in local parallelism and operated at selectable and thus mutually different RF signal amplitudes and/or phasing and/or frequencies and/or voltage-shapes and which nevertheless interact in the plasma reaction volume to result in the said "averaged" effect.

Short description of the figures

The present invention shall now be described by way of examples and with reference to the accompanying drawings. They show:

Fig. 1: Schematically a prior art capacitively coupled RF-plasma reactor,

Fig. 2
to

Fig. 5: four different possibilities of RF-feed to a reactor according to fig. 1 and of arranging a workpiece with respect to larger or smaller electrode, depending on the desired ion bombardment on the surface of the workpiece to be treated,

Fig. 6: the dependency of percentage of RF voltage across the plasma sheath at one electrode from substrate size and depending of whether the substrate or workpiece is deposited on the smaller or on the larger area of the plasma reaction volume confining electrodes at a prior art reactor as shown in figs.

1 to 5,

Fig. 7: in a schematic representation the generic electrode arrangement of a reactor according to the present invention,

Fig. 8: the schematic representation of the generic electrode arrangement of a reactor according to the present invention for explaining the various possibilities of electrical feed to the different electrode arrangements,

Fig. 9: departing from the approach as shown in fig. 7 or 8, schematically the electrode arrangement of the reactor according to the present invention with a preferred shape of sub-electrodes,

Fig. 10: an enlarged view of the reactor according to fig. 9,

Fig. 11: as a function of phase-shift between RF voltages applied to sub-electrode groups at the inventive reactor and as a function of sub-electrode shape the resulting calculated percentage of RF voltage at the plasma sheath of the substrate carrying electrode arrangement,

Fig. 12: the percentage of RF voltage across the plasma sheath at the substrate carrying electrode and as a function of amplitude ratio of RF voltages applied to two groups of inventively provided sub-electrodes,

Fig. 13: in a schematic representation, a preferred construction of the reactor according to the present

invention,

Fig. 14: schematically the bottom view on the electrode arrangement subdivided in bar-shaped sub-electrodes at a reactor according to the present invention,

Fig. 15: in a representation according to fig. 13 the sub-electrode pattern with two-dimensionally arrayed sub-electrode squares,

Fig. 16: in a representation according to fig. 14 or 15 provision of triangular sub-electrodes,

Fig. 17: in a representation according to one of figs. 14 to 16 the provision of groups of honeycomb patterned sub-electrodes,

Fig. 18: departing from a sub-electrode pattern according to fig. 15 the bottom view (a) and cross-sectional view (b) of the sub-electrodes with surface enlarging convex roof shapes,

Fig. 19: in a cross-sectional representation the shapes of a further sub-electrode embodiment with curved surface,

Fig. 20: an enlarged view of a part of the reactor according to the present invention and to fig. 13 with additional preferred features,

Fig. 21: schematically the RF feed of a reactor according to the present invention,

Fig. 22: schematically a first preferred realisation mode of RF feed according to fig. 21,

Fig. 23: schematically a second preferred mode of RF feed according to fig. 21,

Fig. 24: in a schematic bottom view a further structure of sub-electrodes in a centric circular pattern,

Fig. 25: in a schematic representation according to fig. 9 a further preferred embodiment of the inventive plasma reactor with border electrode arrangement,

Figs. 26

to 28: three different distributions of treatment effect on a 400 mm x 400 mm substrate and in dependency of DC bias applied.

Detailed description of the invention with reference to the figures

Before explaining the behaviour of the reactor according to the present invention, let us introduce the notations and the method by recalculating the electrical equilibrium of a classical capacitively coupled RF reactor as shown schematically in fig. 1. Such reactor comprises as was said two electrode arrangements, 1, 2 with respective electrode surfaces A_1 , A_2 which are both capacitively coupled to the plasma 3 within the plasma reaction volume via the respective sheath. The driving RF voltage is generated between the respective electric potentials V_1 and V_2 whereby usually one of these potentials, say V_2 , is reference potential, normally ground potential. The plasma potential V_p is unique because a plasma is a conductor and can be considered conductive as a metal for the driving frequencies considered which are well below the plasma frequency. Capacitive RF coupling between one electrode

and the plasma depends on the sheath thickness. The sheath can thereby be considered as a vacuum capacitor, the thickness thereof varying with RF voltage or potential-drop across the sheath. The most commonly adopted approach consists in describing the sheath thickness as a power law of the local voltage, i.e. potential difference:

$$e_1 = e_2 |V_1 - V_p|^\alpha, \quad e_2 = e_o |V_2 - V_p|^\alpha, \quad (1)$$

where e_1 and e_2 are the respective sheath equivalent thicknesses and α is a coefficient depending on the range of plasma condition and on the type of plasma chemistry being used.

The relation between V_1 , V_2 and V_p is easily derived considering that the two sheaths act as a capacitive divider:

$$(V_1 - V_p) / (V_p - V_2) = (A_2 / e_2) / (A_1 / e_1), \quad (2)$$

$$\text{hence } |V_1 - V_p| / |V_p - V_2| = (A_2 / A_1)^n \text{ with } n = 1 / (1 - \alpha). \quad (3)$$

We recover here the well known power law as first derived by Koenig et al. (H.H. Koenig and L.I. Maissel, IBM J. Res. Dev. 14, 168 (1970)). In this first derivation n was estimated to be around 4 (hence $\alpha = 0.75$). In fact most electronic process conditions correspond more to $n = 1.5$ to 2, ($\alpha = 0.3$ to 0.5). In any case the net result is that most of the RF voltage is found in front of the smaller electrode surface. The result of this calculation is displayed in Fig. 6 where the sheath RF voltage is expressed in percentage of the total RF voltage across the plasma. The calculation is for a square substrate with some reasonable assumptions for the plasma gap (3 cm) and the edge distance (4.5 cm). It appears that when the substrate size exceeds 40 cm, it is impossible with a

classical reactor to develop on one electrode more than 60 % of the RF voltage. It is also impossible to avoid the RF voltage on the larger electrode to be less than 40 % of the total voltage.

As the DC voltage developed across an RF sheath is nearly equal to the local RF voltage amplitude, it is difficult for larger substrates to impose voluntarily a large energy ion bombardment when desired, and it is also difficult to avoid some ion bombardment where such bombardment is not desired. Hence RIE is difficult to implement in large substrate capacitive coupling RF-reactors because only half of the potential self bias will be present in front of the substrate. Recovering this factor implies increasing the RF voltage nearly by 2, hence increasing the RF power by a factor of the order of 3 to 4. On the other hand, avoiding ion bombardment is necessary for processes which are likely to cause plasma induced damages. Since this cannot be reduced by the electrode surface ratio it has to be reduced by reducing the RF amplitude at the expense of a longer process time.

In the figures 2 to 5 the different applications of driving RF voltage to the two electrodes of a capacitively coupled RF reactor are shown, thereby with disposal of the workpiece either on the larger electrode for reduced ion bombardment (fig. 2 and 3) or on the smaller electrode (fig. 4 and 5) for exploiting ion bombardment.

With the help of fig. 7 the principal according to the present invention shall now be explained. Again, the plasma reaction volume 3 of the reactor is confined by two electrode arrangements 10 and 20, principally according to the reactor as shown in fig. 1. In opposition thereto, at least one of the two electrode arrangements, according to fig. 7 one of them, is subdivided into sub-electrodes 12. Subdivision of

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the electrode arrangement 10 into electrically and mutually isolated sub-electrodes 12 may be realised just in one direction x along the electrode arrangement 10 so that the sub-electrodes 12 are of a bar-like shape or may be realised in two directions x and y , so that the sub-electrodes 12 form a two-dimensional pattern.

By this it becomes possible to group the sub-electrodes 12 as shown by the groups A, B, C in fig. 7 and to apply to each of these groups different electric potentials, especially potentials differing generically in amplitude and/or phasing and/or frequency and/or shape, thereby especially such RF potentials. Such different and preferably mutually adjustable driving signals are shown in fig. 7 by V_{11} to V_{13} .

Some general consideration to this inventive concept:

- If both electrode arrangements 10 and 20 are e.g. driven on RF potentials and none is linked to a reference potential as e.g. to ground potential, it is absolutely possible to subdivide both electrode arrangements 10 and 20 into sub-electrodes and to also drive the sub-electrodes of the second electrode arrangement at respectively different potentials (not shown).
- In a most preferred embodiment of one of the electrode arrangements as arrangement 20 being driven on a reference potential the workpiece is deposited adjacent to the unstructured and reference potential driven electrode arrangement, i.e. adjacent to or on electrode arrangement 20 of fig. 7.
- Although it is absolutely possible so as to exploit all possible desired effects of the novel reactor structure to select the different driving voltages at different

frequencies in a most preferred embodiment as proposed presently, the voltages applied differ in amplitude and/or mutual phasing.

- As shown in fig. 7 grouping of the sub-electrodes 12 is preferably realized periodically in that, considered in the direction x, sub-electrodes belonging to the groups A, B, C are arranged periodically alternating. Although this is a most preferred embodiment, it is clear that this periodicity can be omitted or locally interrupted if desired.
- In fig. 7 grouping the sub-electrodes in three respectively RF-driven groups is shown. If desired, more such groups may be realised, but in the today's preferred mode the sub-electrodes are grouped in two differently and further preferably adjustably RF-driven groups.

For the following description we refer to the case according to fig. 7, where the sub-electrodes 12 are grouped periodically in two groups, let us say A and B.

Thereby, the periodicity, i.e. the distance between two subsequent sub-electrodes belonging to the same group should be of the order or less than the extent of the plasma gap according to the distance PG of fig. 7. This will result in the fact that the workpiece is subjected to an "averaged" effect of the several "plasma columns" operated between respective sub-electrodes and the electrode arrangement 20 of fig. 7.

The most general formulation for the electrical signal V_{11} , V_{12} etc. and V_{20} prevailing at the respective sub-electrode groups and, in case of an undivided single counter-electrode, to that counter-electrode 20 according to Fig. 7 may be written as follows:

$$V_{11} = S_1(\tau)$$

$$V_{12} = S_2(\tau)$$

$$V_{20} = S_{20}(\tau)$$

Thereby, S_1 , S_2 and S_{20} denote spectral representations of signals, which spectra may vary in time. It must be pointed out that one of the most important spectral amplitudes is that prevailing for zero frequency, thus representing the DC bias-potential at the respective electrode arrangements. As schematically shown in fig. 8 by respective matching boxes MB_1 , MB_2 and MB_{20} and possibly modulated signal generators G_{11} , G_{12} and G_{20} generating an output signal with a desired spectrum and varying in time as desired, the inventive electrode arrangement may be operated to achieve a large scale of different effects with respect to plasma generation. Thereby, additionally either of the three generators may be omitted and a respective electrode arrangement connected via a respective matchbox to reference potential or by further omission of that matchbox, such electrode arrangement may directly be connected to reference potential.

Further, two or three of the generators shown may be realised as one single generator connected via different matchboxes on the respective electrode arrangements. The skilled artisan will recognise the huge number of control possibilities for the electrical signals V_{nm} , for the minimum number electrode arrangement as shown in fig. 8 and a generalised electrode arrangement of a sub-electrode set 12 with m sub-electrode groups and an electrode 20 also subdivided in n sub-electrode groups.

The matchboxes, which are either passive impedance networks or may possibly include active sources considerably contribute to the formation of the DC bias at the respective elec-

trode arrangements, i.e. the spectral amplitude at zero frequency.

In fig. 9, departing from the example of fig. 7, there is schematically shown a preferred structure of a today's implementation of the reactor according to the present invention. This preferred structure shall be the basis for the analysis as follows. Thereby, the electrode arrangement 10 is subdivided into parallel sub-electrode bars 12, grouped in two groups A and B respectively driven by RF voltages V_{11} and V_{12} with respect to ground potential applied to the electrode arrangement 20. Grouping the sub-electrodes 12 is periodic, as may clearly be seen from fig. 9. The sub-electrodes 12 belonging to the respective groups are interconnected to the respective input by feed-bus 7_A and 7_B .

The sub-electrodes of the group A define for plasma coupling surfaces A_A , whereas the sub-electrodes of group B define such surface A_B . The electrode arrangement 20 is coupled to the plasma reaction volume via surface A_{20} . Both sub-electrode groups are capacitively coupled to the plasma via the respective sheath.

Let us assume:

$$V_{11} = V_0 \exp(i\phi), V_{12} = V_0 \exp(-i\phi) \quad (4)$$

for the two sub-electrode group driving RF voltages, i.e. the two voltages have the same amplitude, but have a mutual phase shift of 2ϕ . Phase ϕ and/or amplitude V_0 may be adjustable or even modulatable. As will be shown, such a reactor according to fig. 7 and more generically according to fig. 8, realised e.g. according to fig. 9 allows to control ion bombardment regardless of workpiece or substrate size and especially in a planar geometry. Indeed, the design according to the figs. 7

to 9 can be extended according to the workpiece extent to be treated.

As may be seen from fig. 9 the sub-electrodes are additionally tailored to enlarge the overall coupling surface $A_{A,s}$ of the electrode arrangement 10. Due to a slope θ of the roof-shaped sub-electrode bars 12, with $\theta = 45^\circ$ according to fig. 9, the surfaces are as follows:

$$A_A = A_B = A_{20}/2\cos(\theta). \quad (5)$$

Note that, as shown in fig. 10, which represents an enlarged part of the reactor structure according to fig. 9, the RF coupling surfaces are evaluated in the central part of the reactor on one unit of the periodic structure. If the workpiece 4 and thus the reactor itself are very large, the border effects can indeed be neglected in this calculation. With respect to accurately controlling even such border effects, we refer to fig. 25 and figs. 26 to 28 as well as to the respective description later on.

Please note that in fig. 10 the plates S_{11} , S_{12} , S_{20} represent the respective parts of electrode surfaces acting as capacitive plates.

The continuity of RF current implies the following equations:

$$(V_o \exp(+i\phi) - V_p) C_{11} + (V_o \exp(-i\phi) - V_p) C_{22} = V_p C_{20} \quad (6)$$

Because $A_A = A_B$ and $|V_{11}| = |V_{12}|$, then, V_p is real, it has a phase centered between V_{11} and V_{12} . The result is expressed in a rather complex form:

$$\tan^2(\phi) = ((X/\cos\theta)^{2/a} - X^2) / (1+X)^2 \quad (7)$$

where
$$X = \cos\phi (V_o/V_p) - 1.$$

This relation was calculated for $\alpha = 0.5$ ($n = 2$) and the results are displayed in fig. 11. Fig. 11 shows the percentage of the driving RF voltage amplitude which is present at the boundary of the sheath facing the bottom electrode 20 on which the substrate 4 is deposited. The calculation was made for four types of saw tooth profile, hence for four values of the angle θ . For zero phase shift, in other words when all electrode groups are driven by the same RF voltage, one recovers the expected results expressed in equation (3). The RF voltage is equally shared when two flat electrodes are facing each other ($\theta = 0^\circ$). When the electrode is corrugated by the saw tooth structure, then the smallest surface electrode is the bottom electrode arrangement 20 and an increasingly large fraction of RF voltage occurs adjacent and facing the work-piece 4. Very impressive is how effective is phase shifting so as to decrease RF voltage in front of the substrate carrying bottom electrode 20. When the two driving voltages are in phase opposition, then the RF voltage in front of the work-piece carrying bottom electrode 20 becomes zero.

Although it is convenient to consider a mere phase shift between the driving voltages for the two electrode groups A and B according to V_{11} and V_{12} , it is not necessary that the voltages on both sub-electrode groups of the array are of the same amplitude, as was explained with the generalised considerations to fig. 8, and even such amplitudes - single at one frequency, or multiple at several spectral frequencies - may vary in time. Thus, amplitude modulation, frequency modulation or phase modulation may be used. Additionally or instead of the varying phasing it is e.g. also possible to vary the amplitude ratio of the driving RF voltages. For the dual periodic array as shown in the figs. 9 and 10, which is one

preferred embodiment of the arrangement according to fig. 8, and still with a phase shift of 2ϕ , varying the one frequency amplitude may be expressed as follows:

$$V_{11} = V_0 \exp(i\phi), \quad V_{12} = aV_0 \exp(-i\phi). \quad (8)$$

in which "a" is a real coefficient between 0 and 1.

As an example we consider the case of a dual periodic array with no phase shift ϕ ($\phi = 0$ in equation (8) but only with a variation of the amplitude of the RF voltage at the RF input for group B, V_{12} . The calculation can be done the same way as above. For illustration, fig. 12 shows the result for a saw tooth dual array with $\theta = 45^\circ$ and $n = 2$. Fig. 12 displays the variation of the plasma RF voltage above the substrate relatively to the amplitude of the main voltage amplitude V_0 when the amplitude of the voltage at V_{12} is varied according to "a" of (8). It is found that the plasma voltage can vary from 15 to 67 % when the amplitude aV_0 of the voltage V_{12} is varied. Even more striking is the variation the self bias of the main electrode. The self bias is calculated by assuming that the plasma sheaths are perfectly rectifying the RF voltage. It is found that the self bias changes sign when the voltage amplitude of V_{12} is varied.

Before reporting some experimental results a preferred form of realisation of the reactor according to the present invention shall be described with the help of fig. 13.

The bars as sub-electrodes 12 of group A are connected to the common bus-bar 7_A and the bars of group B to the common bus-bar 7_B . The bus-bars 7 are respectively connected to RF power inputs 8_A and 8_B . In order to avoid spurious plasma ignition the back of the sub-electrode array and the spaces between the electric connections to the sub-electrode bars 12 are

shielded by spacer shields 9. The substrate 4 is deposited on the opposite electrode 20 which is preferably grounded. All electrodes in this embodiment are cooled or temperature-controlled by a circulating fluid. The fluid is circulating in conducts 11 in the sub-electrode bars 12 of the arrangement 10 and in the base electrode arrangement 20 in conducts 12. The plasma 13 is filling the plasma gap between the electrode arrangements 10 and 20 which gap GP being somewhat larger than the distance P between two adjacent sub-electrodes 12.

As was already noted in the preferred embodiment according to fig. 13, but also according to figs. 7 to 10, the two sub-electrode groups are of equal surface, but it is also possible to consider the case of unbalanced surfaces of the sub-electrode groups surfaces. As also shown in the figs. 9 and 10 the surface of the sub-electrode subdivided arrangement 10 is voluntarily corrugated on the side facing the plasma 13. The purpose of this is to increase the surface of contact between the plasma and the electrode arrangement 10. Note that the profile of a sub-electrode 12 is effective in increasing the contact surface if the geometrical features are wide enough for the plasma to penetrate into the resulting corrugation. In the embodiment according to fig. 13 the sub-electrode bars have again $\theta = 45^\circ$. The surface of contact between the electrode arrangement 10 and the plasma 13 is therefore increased by a factor of $\sqrt{2}$ compared to the flat base electrode arrangement 20.

In a further preferred embodiment the base electrode 20 may be construed as a chuck for holding by suction flat workpieces 4 as glass plates to be treated. To realize such a chuck there is (not shown in fig. 13) realized within electrode arrangement 20 a system of suction channels which abut in a multitude of suctioning holes at the upper surface of electrode 20 to snugly hold the workpiece 4 during treatment, or

there is provided an electrostatic chuck.

Experiments were performed on a reactor construed as shown in fig. 13. Both extremes with respect to RF driving were performed, namely where both electric inputs 8_a and 8_b were driven together and thus $V_{11} = V_{12}$ (see fig. 9) and where one of the inputs 8_b or 8_a was grounded, thus realizing $a = 0$ according to (8). The self bias potential and the RF driving amplitude were measured. As seen in Table 1, the results are qualitatively very satisfactory. In particular one observes a spectacular change of signum of the self bias when the electrode equivalent contact surface is reduced by a factor of 2 when varying the RF voltage applied to one sub-electrode group from nominal to zero. The absolute value of RF self bias does not match the theoretical estimation. This is mainly due to the fact that the measurements were performed on a rather small reactor of $500 \times 500 \text{ mm}^2$. The calculation for an infinite reactor as shown in fig. 12 must be corrected to take into account the contributions of the reactor edges to RF coupling. This was done in an approximate way in Table 1. Nevertheless, the drastic variations of the DC bias are astonishing. The RF bias of the processing plasma in front of the workpiece can be drastically changed by relative variation of RF input voltages on the sub-electrode groups.

SET UP	MEASURED ON REACTOR			RATIO CALCULATED	
	V_0 RF	Self bias	ratio	corrected	calculated
two in parallel	306 V	+ 244 V	0.79	0.62	0.33
one grounded	360 V	- 142 V	-0.39	-0.59	-0.71

Table 1: Comparison experiment-theory for a dual array with 45° saw tooth. The corrected value is derived from a calculation as above but roughly accounting for the edge effects which are far to be negligible in relatively small reactors.

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The sub-electrode design according to figs. 9, 10 and 13 is very simple. It is the most simple periodic structure. From the bottom it appears as parallel stripes as shown in fig. 14 with alternated connections to the two RF inputs.

Such a periodic design can also be made periodic in two dimensions, x / y of fig. 7. Such an example is shown schematically in fig. 15 for a square-shaped sub-electrode 12.

Similarly, a dual array of triangular sub-electrodes 12 can be made as schematically shown in fig. 16. An even more sophisticated approach is shown in fig. 17 where a triple array with three RF inputs and three groups A, B, C of sub-electrodes is realized. Again, the three corresponding driving RF voltages or more generic signal spectra can be out of phase and/or of different amplitudes, possibly even of different frequencies and/or voltage-shapes, the signals may have different spectra.

The periodic structure of the sub-electrode array can also introduce features with respect to electrode surface as does the tooth pattern which was described. A diamond shape as shown in fig. 18 increases the RF capacitive coupling surface of each sub-electrode and may be applied to different sub-electrode structures e.g. as shown in the figs. 15 to 17. The sub-electrode profile can also be rounded as shown in cross-section in fig. 19. One of the only limitations for the design rules of the electrode array structure is that when shaping the sub-electrode units, hollow volumes or volumes open to the plasma reaction volume such as holes, grooves or slots shall be wider than twice sheath thickness or dark space distance so that the plasma penetrates deeply into such recesses. In a typical plasma process the sheath thickness is a few mm, hence it is reasonable to assume that no hollow in-

trusion on the surface of electrode arrangement 10 should be narrower than about 1 cm if such intrusion shall add to the active coupling surface of such electrode.

Considering the reactor according to the present invention and as most generically shown in fig. 8, it must be stated that laying the workpiece flat on the bottom horizontal electrode arrangement 20 is the most convenient approach, but the same design can be realized vertically or with the substrate and electrode arrangement 20 at top if appropriate workpiece and especially substrate holding is realized. Such different geometric arrangement can be considered with an eye on particle control.

Some preferred additional features shall be explained with an eye on fig. 20 which shows an enlarged cross-sectional view of the sub-electrode array. In order to limit the capacitive coupling between the sub-electrodes of the e.g. two sub-electrode groups the gaps 23 between adjacent sub-electrodes can be provided with spacers 24. These spacers can be made of an insulating material such as of ceramic or of a metal, either at floating potential or at a defined potential intermediate the potentials applied to the adjacent sub-electrodes. Similarly, a shield 26 above the sub-electrodes reduces the capacitive coupling, either between the sub-electrodes and/or from the sub-electrodes to the backing ground plate 25. This shield 26 can be continuous, but then it shall be made of an insulating material such as of ceramic or if it is metallic, it shall be interrupted as shown in fig. 20. Several shielding layers can be interposed to improve capacitive decoupling. In fig. 20 a second shield 27 is shown to improve decoupling between the sub-electrode array and the backing ground plate 25. The shield 27 is actually a grid to allow gas to flow therethrough.

This introduces another advantage of the sub-electrode array. One can take advantage of the spacings or gaps 23 between the sub-electrodes to allow a gas 31 to flow between the sub-electrodes and into the reaction volume. For this, a process gas 31 is introduced through a piping 28 into the area behind the sub-electrode array. Means may be provided to uniformly distribute the inlet gas 31 to the gas outlets 23 as e.g. realized by the grid shield 27.

Some further considerations to the RF feed system:

From the sub-electrode groups provided, at least one with at least one sub-electrode is to be RF-voltage driven.

The inputs to the groups of sub-electrodes for RF voltage shall be realized through vacuum feed-throughs 41 as shown in fig. 20. Thereby, as is customary for RF feed, as was discussed there is provided a matching box 42 matching the output of amplitude and/or phase adjustable or modulatable RF generators 43 and 44 which generate narrow-band or wide-band signal spectra. Thus, one generator 44 may e.g. be adjustable in its sole amplitude of its output RF signal whereas the second generator 43 may be adjustable in phasing at a single spectral frequency. Phase shift of the two RF signals input to two or more groups of the sub-electrode array may also be performed within the matching box 42. For the skilled artisan there are many different ways for implementing the RF drive to the reactor according to the present invention and as shown in fig. 8.

A today preferred technique is schematically shown in fig. 22. There is provided one RF oscillator 47, the one frequency RF output thereof being led via an adjustable phase shifter unit 48 on a power amplifier 49 and additionally directly on the input of a second power amplifier 50. Preferably, the

amplifiers 49 and 50 are tailored to accept large reflected power and they are coupled to the RF inputs of the reactor via simple passive matching circuitry in order to roughly match the plasma impedance to the generator impedance. Another preferred design is shown in fig. 23 where two amplifier output stages 55 and 56 are driven by the same - one frequency - RF oscillator but provide for independent adjustment of amplitude and/or phasing of the output RF voltage. The output of the amplifier stage 55 is coupled through a matchbox to the primary winding 51 of a transformer. The secondary winding 60 of the transformer provides an RF voltage difference between the group inputs to the sub-electrode groups according to the present invention. The central point of secondary winding 52 is connected via a matchbox 54 to the output of the second amplifier output stage 56. Phase control and/or amplitude control is preferably performed at amplifier stages 56 and/or 55.

Thus, the most generic aspect of the reactor according to the present invention is to provide at least one sectioned electrode. In spite of the preferred examples described it might be interesting not to evenly space the sub-electrodes e.g. for resolving general etching problems with respect to homogeneous treatment distribution. Sub-electrodes of annular shape or of frame-like shape may be arranged around a central axis. Such a centric grouping of the sub-electrodes is schematically shown in fig. 24.

Further, it must be pointed out that it is absolutely possible to operate one or the other or more than one of the sub-electrode groups at a predetermined non-RF potential such as on DC. It is further evident that the RF generator arrangements with phase and amplitude and possibly even frequency adjustment may be realized digitally thereby providing a power amplifier output stage to feed the sub-electrode group.

inputs. Also, as the inventive concept allows for separate independent inputs, it is well suited to drive the different sub-electrode groups by differently shaped voltages according to different signal spectra, briefly, one has complete freedom to operate the sub-electrode groups at any electric signal desired and mutually independently.

It is further to be pointed out that e.g. for RIE applications the reactor according to the present invention and with corrugated surface enlarging sub-electrodes may be operated with all sub-electrode groups on the same RF voltage whereby the mere fact of enlarged electrode surface at the structured electrode arrangement significantly improves ion bombardment of the substrate deposited on the counter electrode arrangement according to arrangement 20 of fig. 7. In RIE application and making use of a reactor as shown in fig. 13, thereby feeding all sub-electrode groups with the same RF voltage, it was possible to treat glass substrates of 370 x 370 mm extent by carbon deposition with a coating uniformity according to maximum deviations of 5 % from the desired thickness. After treatment, the reactor was cleaned by an oxygen plasma.

Further consideration must be given to cooling and heating of the substrate to be treated. Thus, and according to electrode 20 of fig. 13, cooling/heating is preferably accurately controlled so as to reach different substrate temperatures, depending whether the substrate is coated as by chemical vapour deposition in the inventive reactor or is etched. For etching substrates, and especially substrates which are provided with a photolacquer layer, the substrate temperature is to be maintained preferably below photolacquer melting temperature. Thus, for such operation, the substrate, e.g. on electrode 20 of Fig. 13, is cooled by the cooling system 12 to a temperature in the range of 40°C to 80°C.

If the reactor is used for layer deposition on the substrate as for performing plasma enhanced vapour deposition, then the substrate is preferably heated, e.g. to about 200°C. This considerably improves the quality of the deposited layers in that the layers are deposited with reduced stress, necessitating no additional heat treatment. It is thereby rather uncommon to heat the substrates during PECVD to such relatively high temperatures.

Looking back on Fig. 7, of V_{11} , V_{12} , V_{13} ...

- at least one comprises an effective RF spectrum
- all signals at a one-side electrode (substrate or no-substrate electrode) may be the same
- DC, AC, pulsating ramp and all kinds of signals resulting from super-position may be applied, as DC + AC + ramp.

Especially in the embodiment according to Fig. 9 the sub-electrode groups may be driven at one common signal whereby for such a case the sub-electrodes might be conductively linked to form a corrugated electrode area so as to enlarge surface area. The same is valid for structures as shown in Figs. 14 to 19.

Up to now we did not describe any features at the inventive reactor to deal with border effects with respect to homogeneity of substrate treatment. In fig. 25 there is shown an inventive reactor according to fig. 9 and electrically driven generically as was discussed in connection with fig. 8, whereby there is provided besides the two groups of sub-electrodes driven at V_{11} , V_{12} a border electrode 50 of e.g. triangular cross-sectional shape as shown. This border electrode 50 is generically electrically operated via a matchbox MB_g and a generator G_g . Thereby, again, the generator G_g may generate a signal of predetermined spectrum, possibly frer-

quency, phase or amplitude modulated, thereby may generate a single frequency signal or such generator G_3 may be just omitted, just maintaining the matchbox connected to ground potential. Again the matchbox considerably contributes to the DC bias according to the zero spectral frequency amplitude of the signal V_{30} prevailing at border electrode 50.

By means of the border or peripheral electrode 50, preferably surrounding the subdivided electrode arrangement 10, and either passively connected preferably via a matchbox to reference potential or actively driven by an additional generator, a considerable improvement with respect to treatment uniformity is reached and especially with respect to etching uniformity at a substrate. Thereby, the border electrode 50 may even be left on floating potential. Preferred operation of the border electrode 50 is nevertheless via a matching box connected to reference potential with or without additional generator G_3 .

A reactor according to fig. 25 was operated as follows:

- V_{11} : RF; 13,56 MHz, 0 V DC bias,
1kV RF power
- V_{20} : linked to ground potential via a passive
adjustable matchbox
- V_{30} : connected to ground potential via a passive
adjustable matchbox MB_3

In a CF_4/SF_6 a-Si: H-atmosphere, at 5×10^{-2} mbar, the distribution of etching effect on 400 mm x 400 mm substrates was tested.

Fig. 26 shows the distribution at:

DC bias of V_{20} : -215 V

- 27 -

DC bias of V_{80} : +107 V
DC bias of V_{11} , V_{12} : 0 V

Fig. 27 shows the distribution at:

DC bias of V_{20} : -320 V
DC bias of V_{80} : -83 V
DC bias of V_{11} , V_{12} : 0 V

Fig. 28 shows the distribution at:

DC bias of V_{20} : -312 V
DC bias of V_{80} : +3 V.
DC bias of V_{11} , V_{12} : 0 V

Therefrom, it is clearly seen that the distribution of process effect along the workpiece may accurately be adjusted by appropriately selecting the respective DC bias signal applied to either of the electrodes.

Claims:

1. A capacitively coupled RF plasma reactor comprising:
 - a first and a second extended electrode arrangement mutually and substantially constantly spaced and confining a plasma reaction volume
 - at least one of said first and of said second electrode arrangements being subdivided into electrically mutually isolated sub-electrodes
 - a first group of said sub-electrodes being connected to a common first electric input
 - a second group of said sub-electrodes being commonly connected to a second electric input
 - said first and said second electric inputs being independent.
2. The reactor of claim 1, wherein said sub-electrodes are formed by sub-electrode bars.
3. The reactor of claim 1 or claim 2, wherein said at least one electrode arrangement is subdivided in a two-dimensional pattern of said sub-electrodes.
4. The reactor of one of claims 1 to 3, wherein said at least one electrode arrangement is subdivided into frame-like or annular sub-electrodes.
5. The reactor of one of claims 1 to 4, wherein considered in at least one direction along said at least one electrode arrangement sub-electrodes of said groups are arranged in a

periodically alternating pattern.

6. The reactor of one of claims 1 to 5, wherein said sub-electrodes have surfaces pointing towards the second of said two electrode arrangements which are convexly or concavely enlarged.

7. The reactor of one of claim 1 to 6, wherein said first and second electrode arrangements are substantially planar parallel electrode arrangements.

8. The reactor of one of claims 1 to 7, wherein said first electric input, said second electric input and a further electric input to the other of said first and of said second electrode arrangements are respectively connected to a generator arrangement generating at at least two of said inputs equal electric signals.

9. The reactor of one of claims 1 to 8, wherein said first electric input, said second electric input and a further electric input to other of said first and of said second electrode arrangement are connected to respective generator arrangements, each being respectively selected from the group consisting of:

- a generator arrangement consisting of a passive impedance element matchbox
- a generator arrangement consisting of an active signal generating arrangement with or without a passive impedance element matchbox
- a generator arrangement generating at its output exclusively a reference DC potential

and wherein said active generator generates one of the fol-

lowing signals:

- a DC signal
- an AC signal of a predetermined or adjustable frequency spectrum, said spectrum being one of constant in time and of varying in time with respect to at least one of spectral amplitudes, frequency distribution and phasing.

10. The reactor of one of claims 1 to 9, wherein at least two of said first electric input, said second electric input and of the further electric input to the other of said first and of said second electrode arrangements are connected via equal matchboxes to different electric signal generators or are connected via different matchboxes to a common electric signal generator.

11. The reactor of one of claims 1 to 10, wherein said at least one of said first and of said second electrode arrangements are subdivided in more than two groups of sub-electrodes.

12. The reactor according to one of claims 1 to 11, further comprising at least one border electrode, electrically isolated from and adjacent to said at least one of said first and of said second electrode arrangements.

13. The reactor of claim 12, wherein said border electrode surrounds said at least one of said first and of said second electrode arrangement.

14. The reactor of claim 8, further comprising a border electrode adjacent to said at least one of said first and of said second electrode arrangements and comprising a still further electric input, said first, second, further and still

further electric inputs being respectively connected to a generator arrangement generating at at least two of said inputs equal electric signals.

15. The reactor according to claim 9, further comprising a bordering electrode, bordering said at least one of said first and of said second electrode arrangements and comprising a still further electric input, said first, second, further and still further inputs being respectively connected to a generator arrangement selected as one of said group.

16. The reactor of claim 10, further comprising a border electrode adjacent to said at least one of said first and of said second electrode arrangements and comprising a still further electric input, at least two of said first, second, further and still further electric inputs being connected via equal matchboxes to different electrical signal generators or via different matchboxes to one common electric signal generator.

17. The reactor of one of claims 1 to 16, wherein at least one of said electrical inputs being connected to an RF signal generator, the output signal thereof being adjustable with respect to amplitude and/or phasing and/or frequency and/or signal shape.

18. The reactor of one of claims 1 to 17, wherein at least two of said first, second and of the further electric inputs connected to the other one of said first and of said second electrode arrangement are connected to an RF generator arrangement, whereas mutual amplitude ratio and/or phasing is adjustable.

19. The reactor of one of claims 1 to 18, wherein the distances between neighbouring sub-electrodes is smaller than

dark space distance of a plasma generated in said reaction volume.

20. The reactor of one of claims 1 to 19, further comprising a channel arrangement at at least one of said first and said second electrode arrangements connected to a temperature control fluid source.

21. The reactor of one of claims 1 to 20, further comprising a gas distribution chamber on the backside of said at least one electrode arrangements with a gas inlet and communicating via intermediate spaces separating said sub-electrodes from each other with said reactor volume.

22. The reactor of one of claims 1 to 21, further comprising shielding members at least one of between adjacent sub-electrodes and of behind said sub-electrode.

23. A capacitively coupled RF plasma reactor comprising:

- a first and a second extended electrode arrangement mutually and substantially constantly spaced and confining a plasma reaction volume
- at least one of said first and of said second electrode arrangements comprising a corrugation pattern so as to considerably enlarge the surface area of said electrode.

24. A method for controlling ion bombardment ratio of ion bombardment on one electrode surface and ion bombardment on a second electrode surface, said electrode surfaces being formed by a first and a second electrode arrangement confining a plasma reaction volume of a capacitively coupled RF plasma reactor comprising the steps of:

- subdividing at least one of said first and of said second electrode arrangements into mutually electrically isolated sub-electrodes
- applying to at least one of said sub-electrodes an electric potential which is independent from an electric potential applied to at least one other sub-electrode
- mutually adjusting said first and second electric potentials to control ion bombardment ratio.

25. The method of claim 24, further comprising the step of temperature controlling at least one of said first and of said second electrode arrangements.

26. The method of claim 25, further comprising the step of controlling the ion bombardment so as to etch a substrate on one of said first and second electrode arrangements and controlling the temperature of said substrate to be in the range of 40°C to 80°C (both limits included).

27. The method of claim 25, thereby controlling said ion bombardment ratio to perform layer deposition on a substrate provided at one of said first and of said second electrode arrangements and controlling the temperature of said substrate to be above 150°C, preferably at about 200°C.

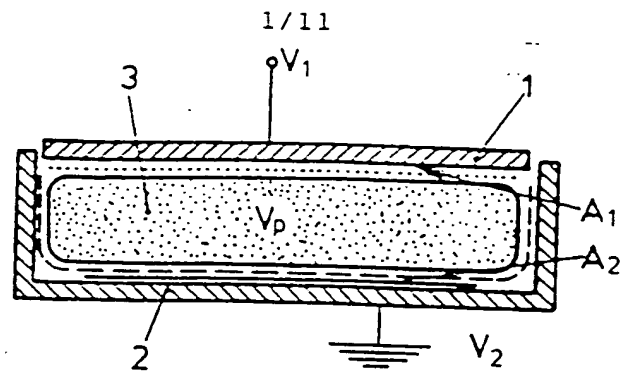


FIG. 1

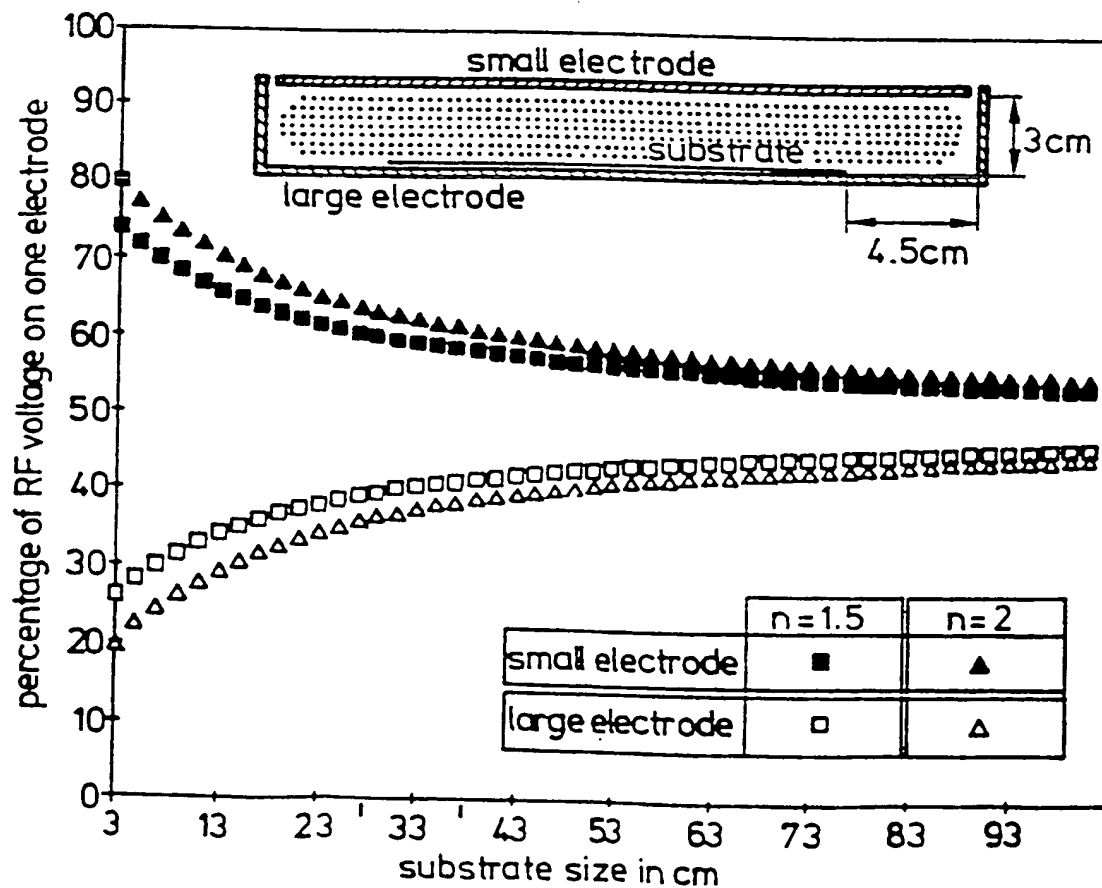
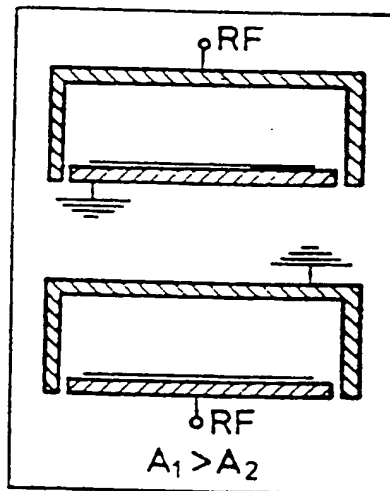
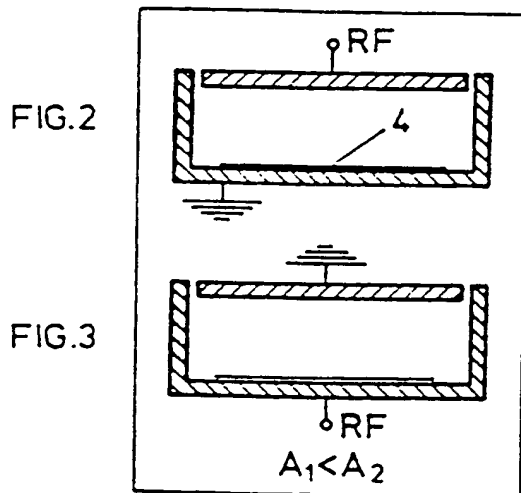
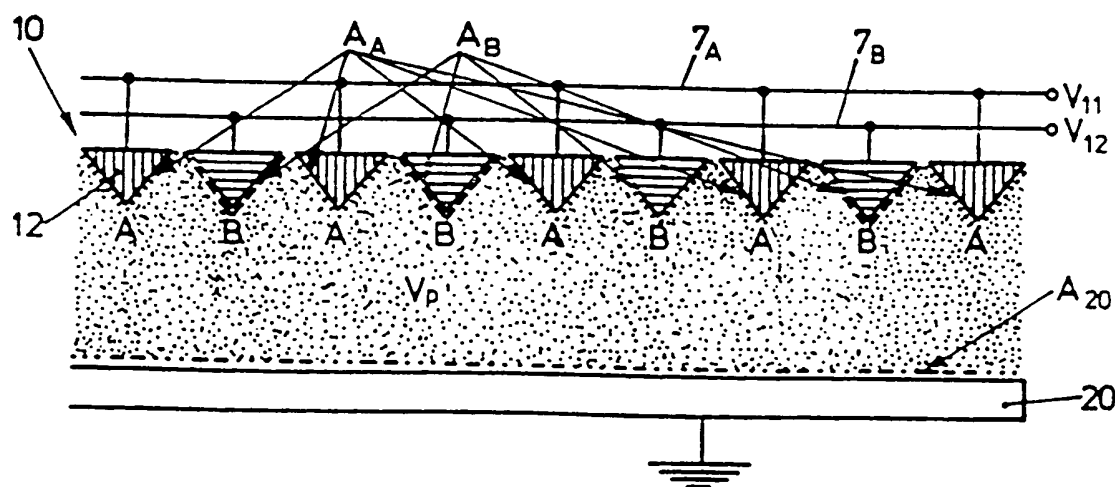
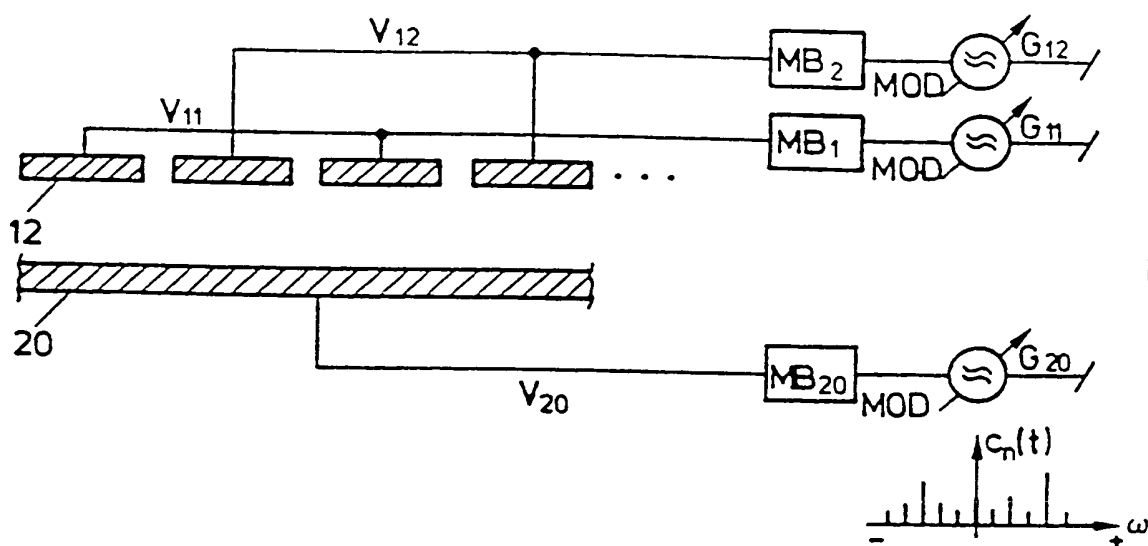
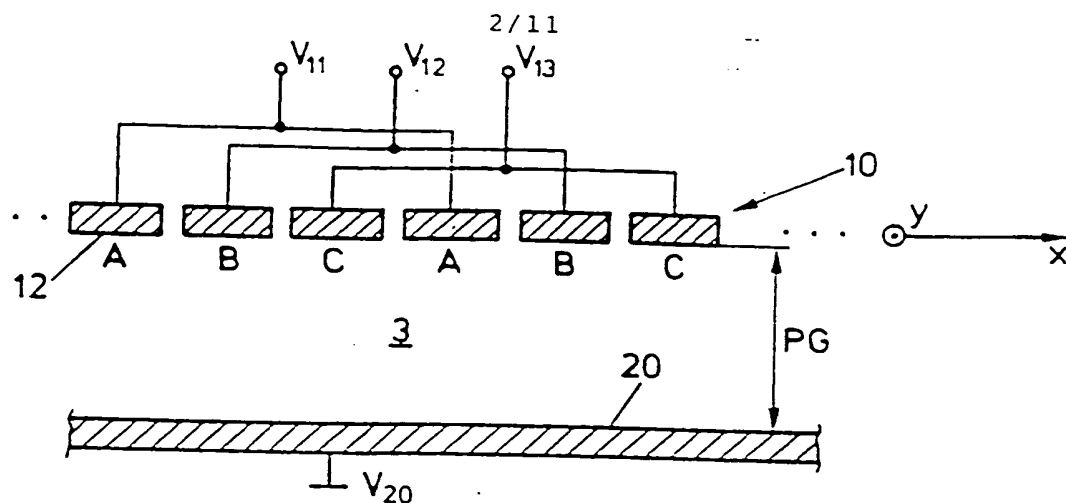


FIG. 6



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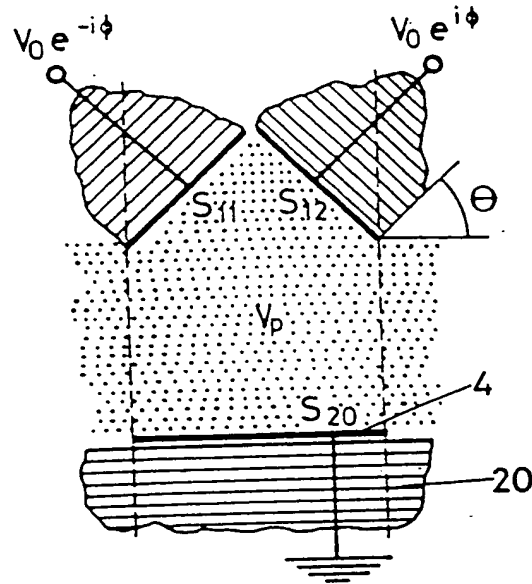


FIG.10

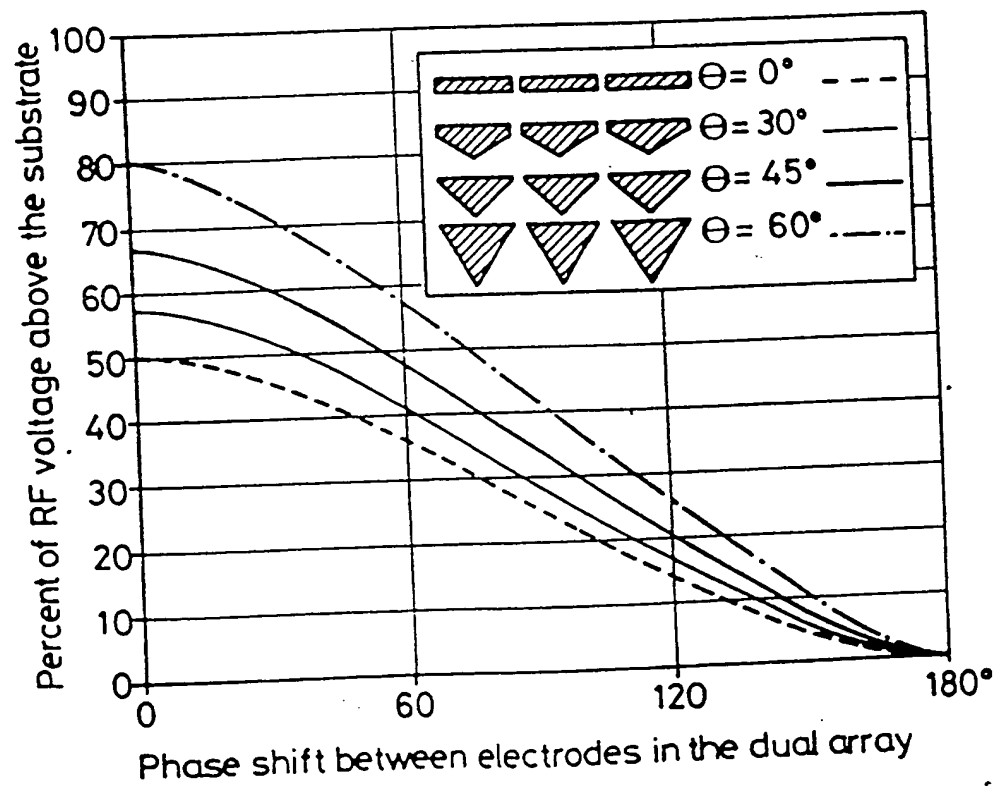


FIG.11

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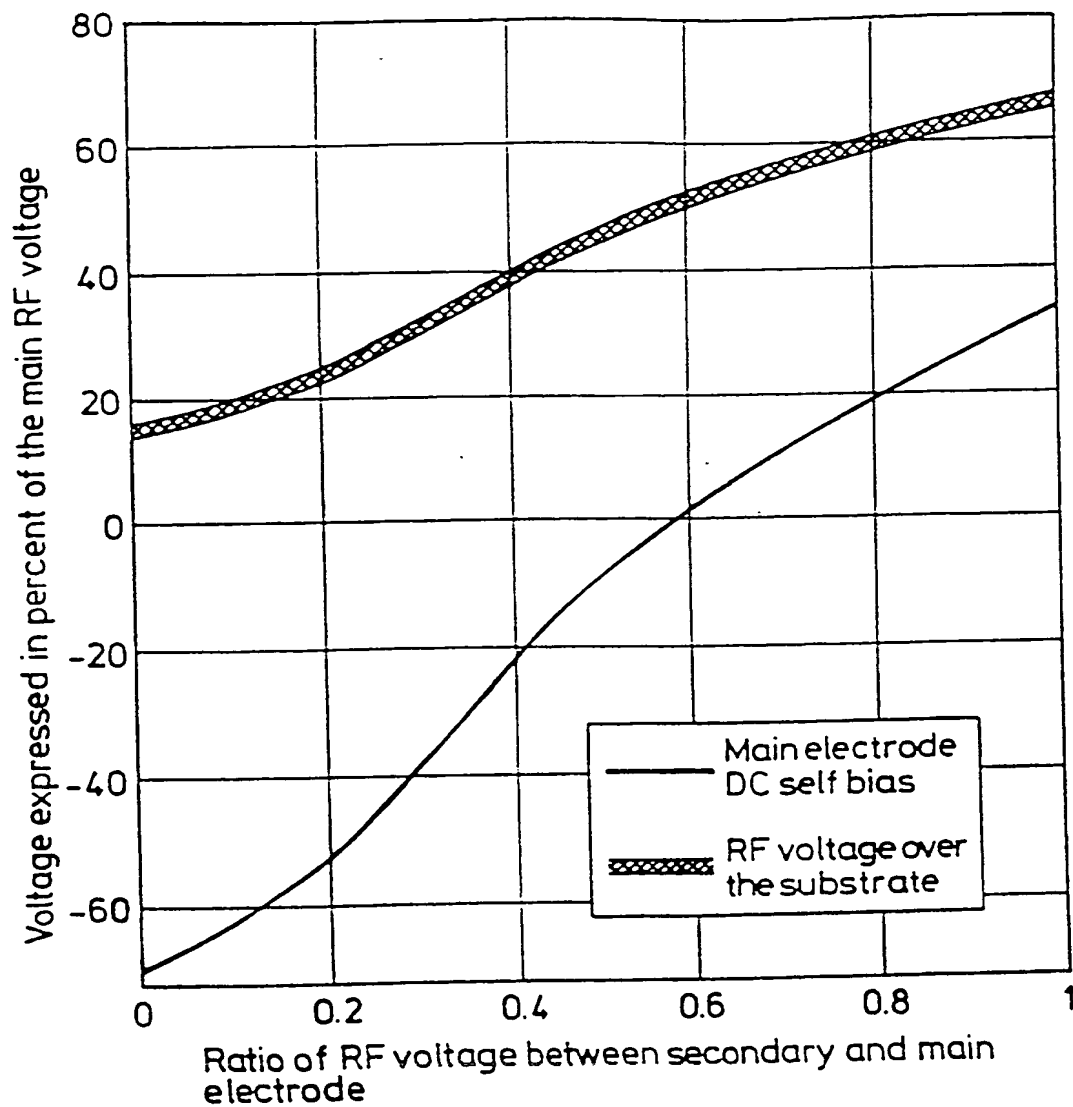


FIG.12

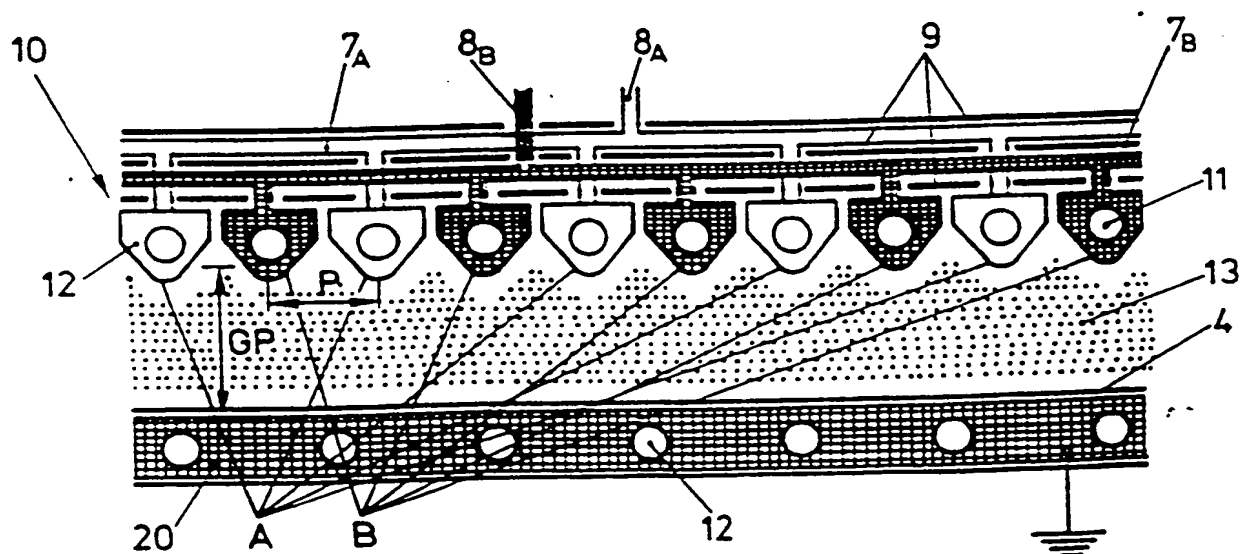


FIG.13

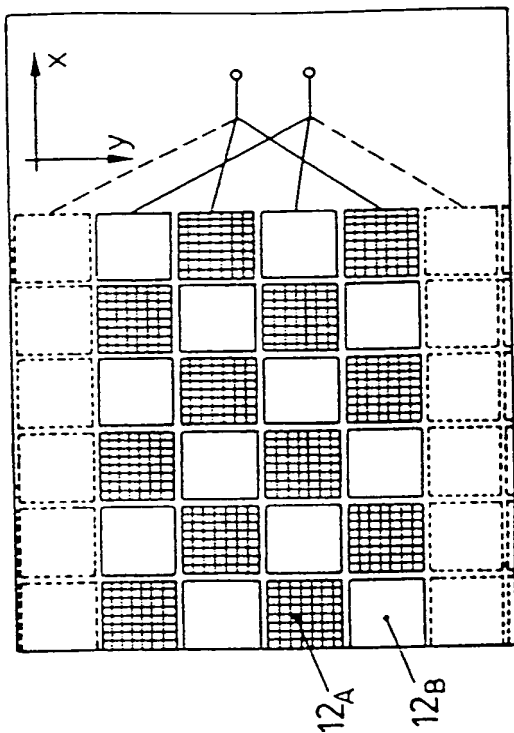


FIG. 15

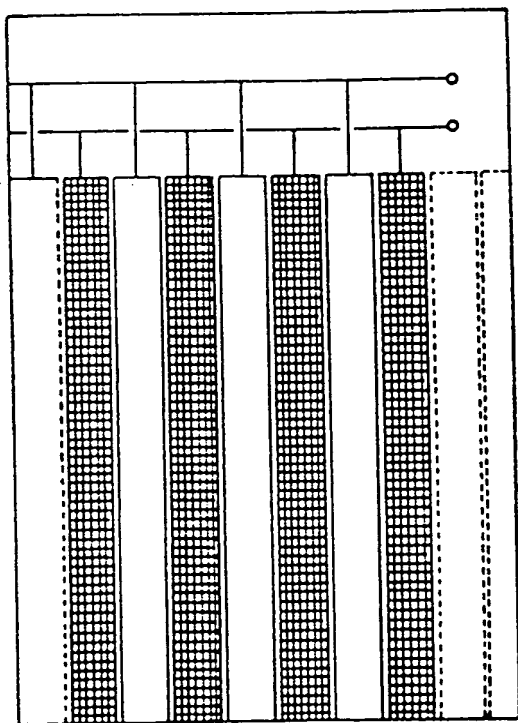


FIG. 14

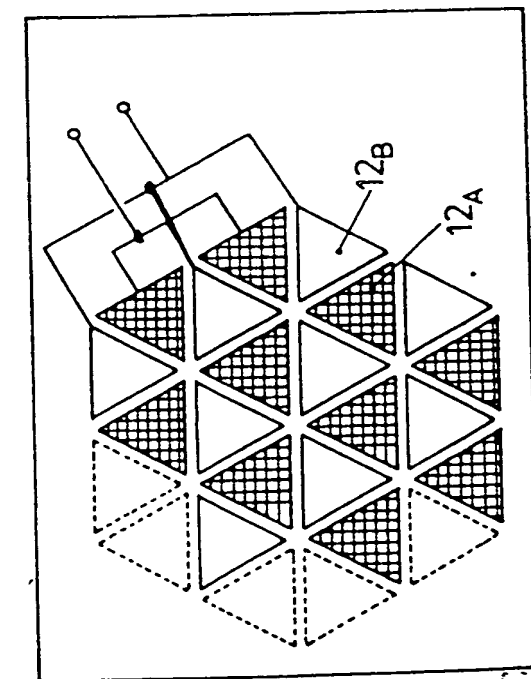


FIG. 16

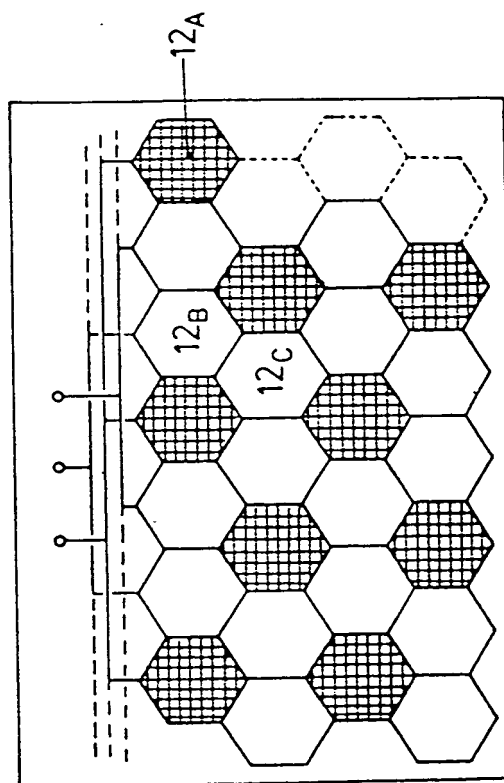


FIG. 17

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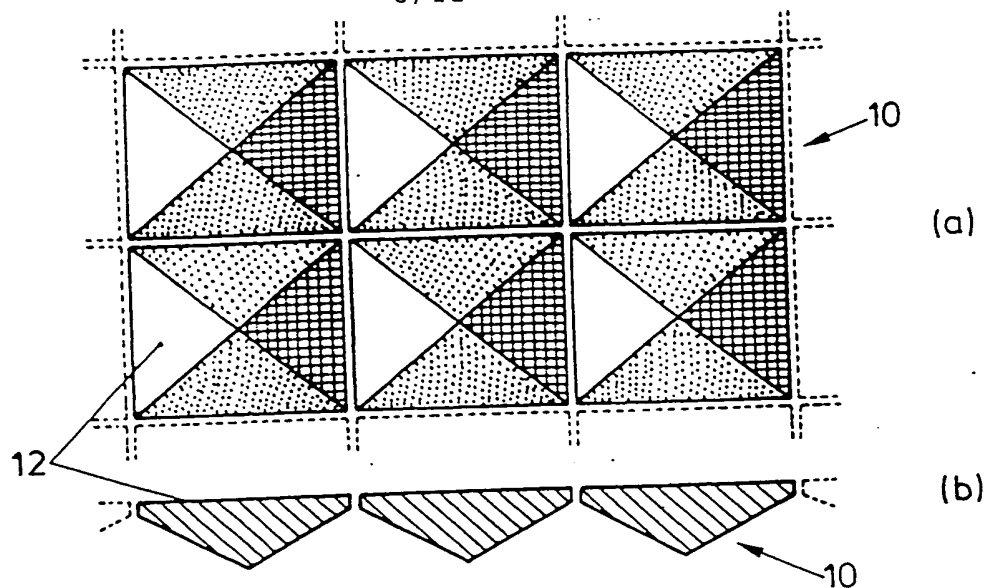


FIG.18

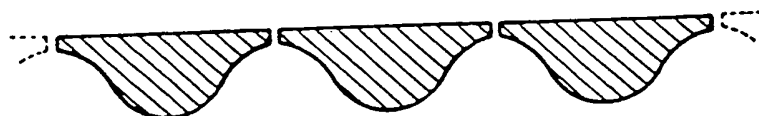


FIG.19

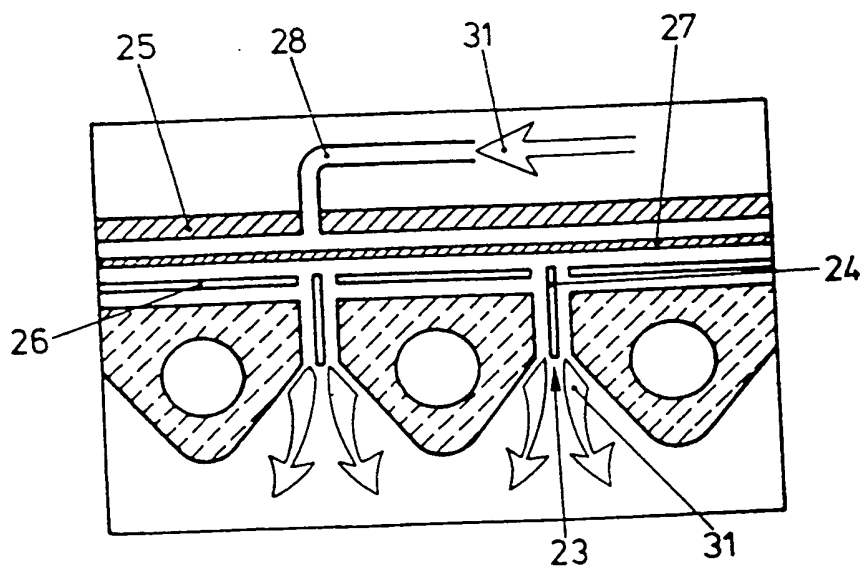


FIG.20

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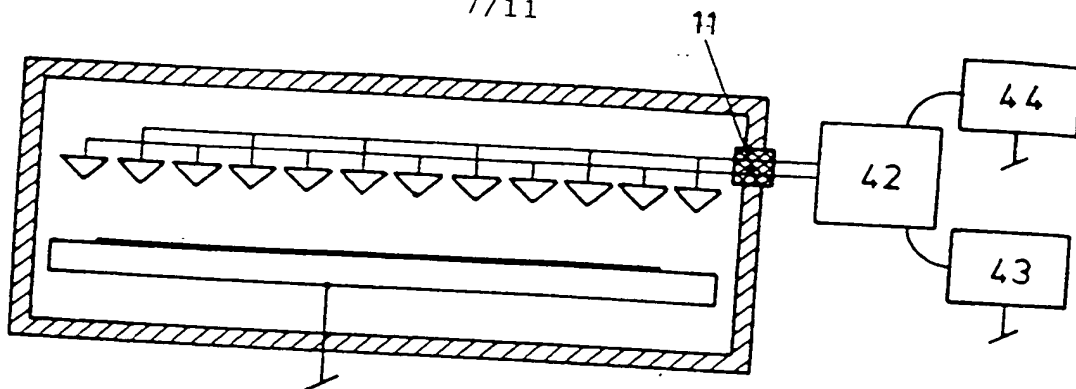


FIG. 21

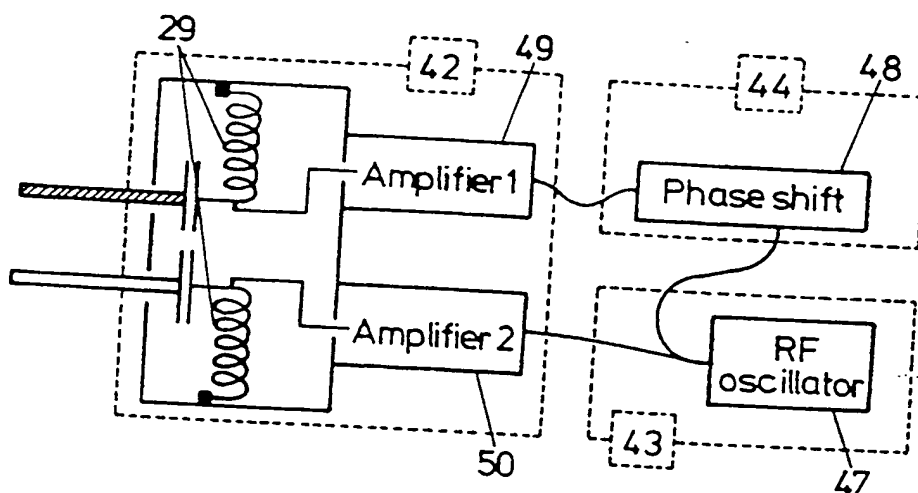


FIG. 22

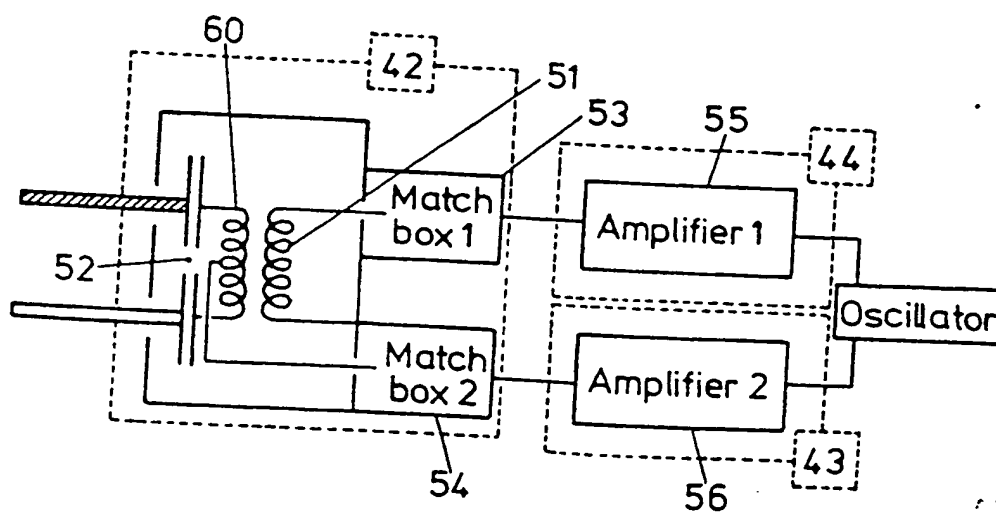


FIG. 23

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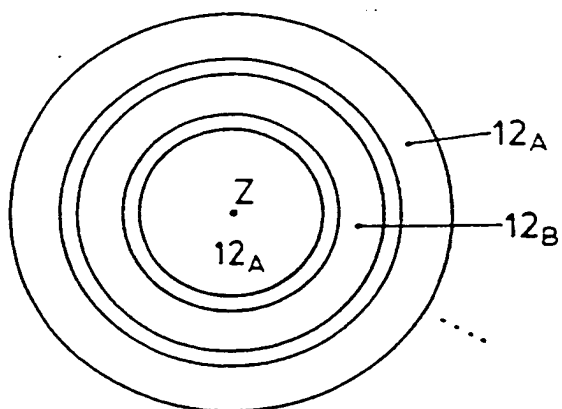


FIG. 24

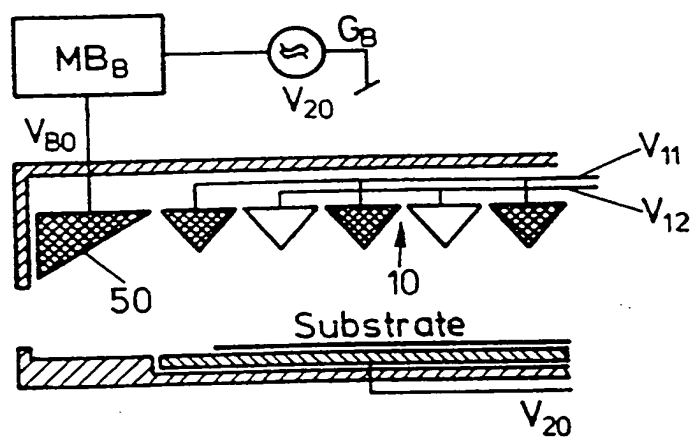
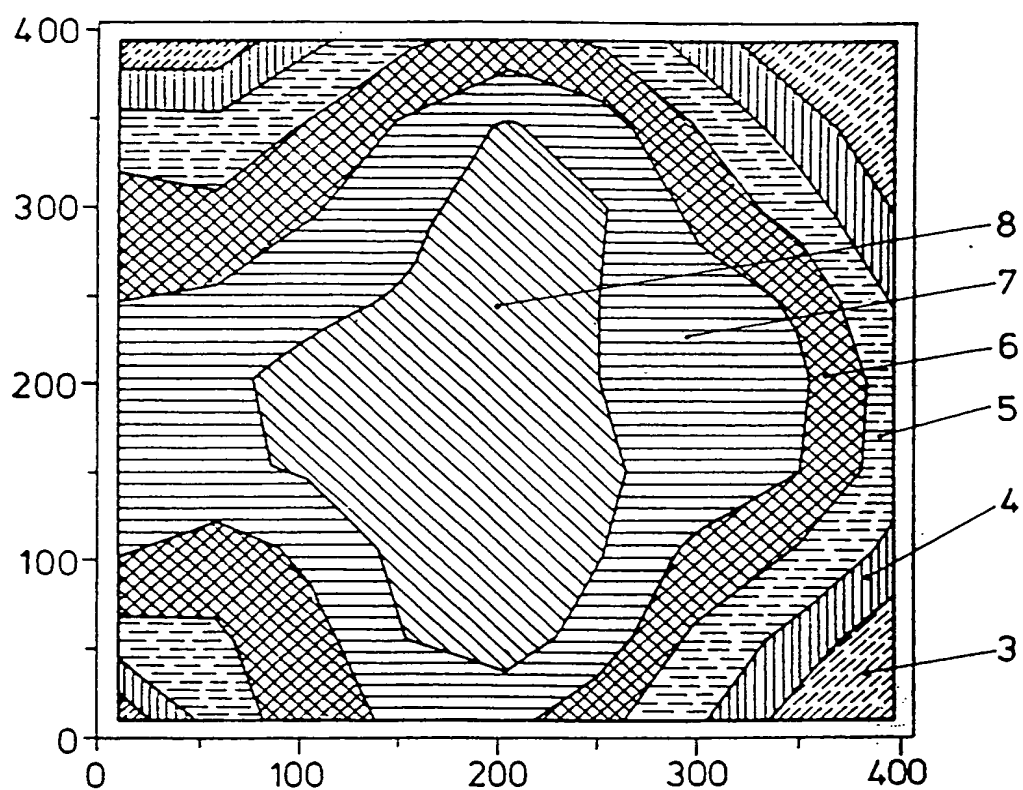


FIG. 25

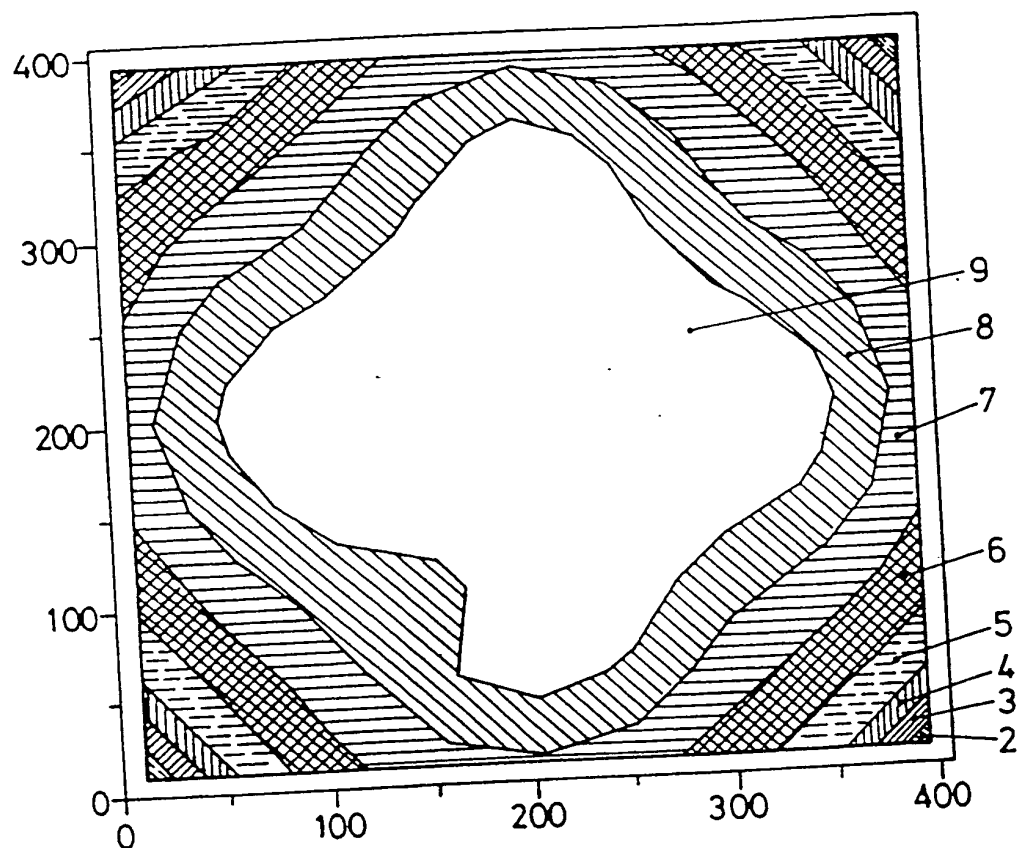
9/11



	<u>nm:</u>
1	+14 -- +18 %
2	+11 -- +14 %
3	+7.2 -- +11 %
4	+3.6 -- +7.2 %
5	0 -- +3.6 %
6	-3.6 -- 0 %
7	-7.2 -- -3.6 %
8	-11 -- -7.2 %
9	-14 -- -11 %
10	-18 -- -14 %

FIG. 26

10/11



nm:		
1		+14 -- +18 %
2		+11 -- +14 %
3		+7.2 -- +11 %
4		+3.6 -- +7.2 %
5		0 -- +3.6 %
6		-3.6 -- 0 %
7		-7.2 -- -3.6 %
8		-11 -- -7.2 %
9		-14 -- -11 %
10		-18 -- -14 %

FIG. 27

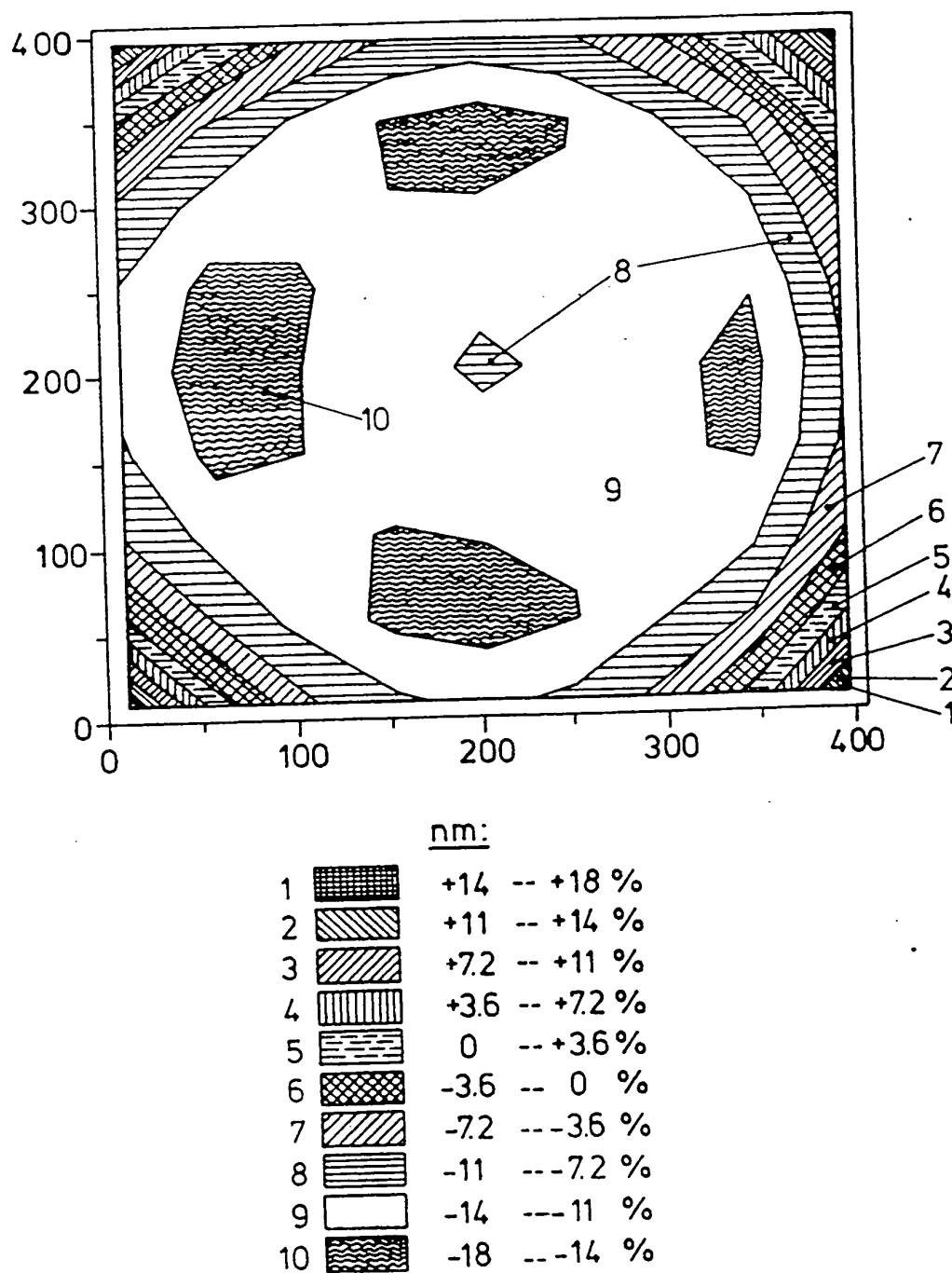


FIG.28

INTERNATIONAL SEARCH REPORT

A. CLASSIFICATION OF SUBJECT MATTER IPC 6 H01J37/32		International Application No PCT/IB 98/00043
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) IPC 6 H01J		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used)		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
P, X	US 5 609 690 A (WATANABE SYOUZOU ET AL) 11 March 1997	1,3-6, 8-13, 17, 18, 24 23
Y	see column 1, line 14 - line 45; figures 21, 22	
X	see column 3, line 49 - column 5, line 13; figures 1-3, 10-12 & PATENT ABSTRACTS OF JAPAN vol. 095, no. 011, 26 December 1995 & JP 07 226395 A (MATSUSHITA ELECTRIC IND CO), 22 August 1995, see abstract	1, 24
Y	--- PATENT ABSTRACTS OF JAPAN vol. 018, no. 199 (E-1534), 7 April 1994 & JP 06 005522 A (MITSUBISHI HEAVY IND LTD), 14 January 1994, see abstract ---	23
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<input checked="" type="checkbox"/> Further documents are listed in the continuation of box C.		
<input checked="" type="checkbox"/> Patent family members are listed in annex.		
* Special categories of cited documents :		
"A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier document published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. "&" document member of the same patent family		
Date of the actual completion of the international search 25 March 1998		Date of mailing of the international search report 02/04/1998
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel: (+31-70) 340-2040, Tx: 3: 551 epo nl, Fax: (+31-70) 340-3016		Authorized officer Schaub, G

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INTERNATIONAL SEARCH REPORT

Int. Application No
PCT/IS 98/00043

C. (Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No
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X	PATENT ABSTRACTS OF JAPAN vol. 096, no. 007, 31 July 1996 & JP 08 078187 A (FUJITSU LTD: FUJITSU VLSI LTD), 22 March 1996, see abstract ---	1,3,24
A	DE 44 04 077 A (LICENTIA GMBH) 10 August 1995 see column 5, line 52 - column 6, line 25: figure 4 -----	1,24

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INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No.

PCT/IB 98/00043

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EP 0099174 A	25-01-84	US 4474659 A JP 58223400 A US 4863577 A US 4806225 A	02-10-84 24-12-83 05-09-89 21-02-89
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